

Alpine Naturgefahren und Herausforderungen für alpine Infrastruktur in der Zukunft

Bauen mit Holz im alpinen Raum

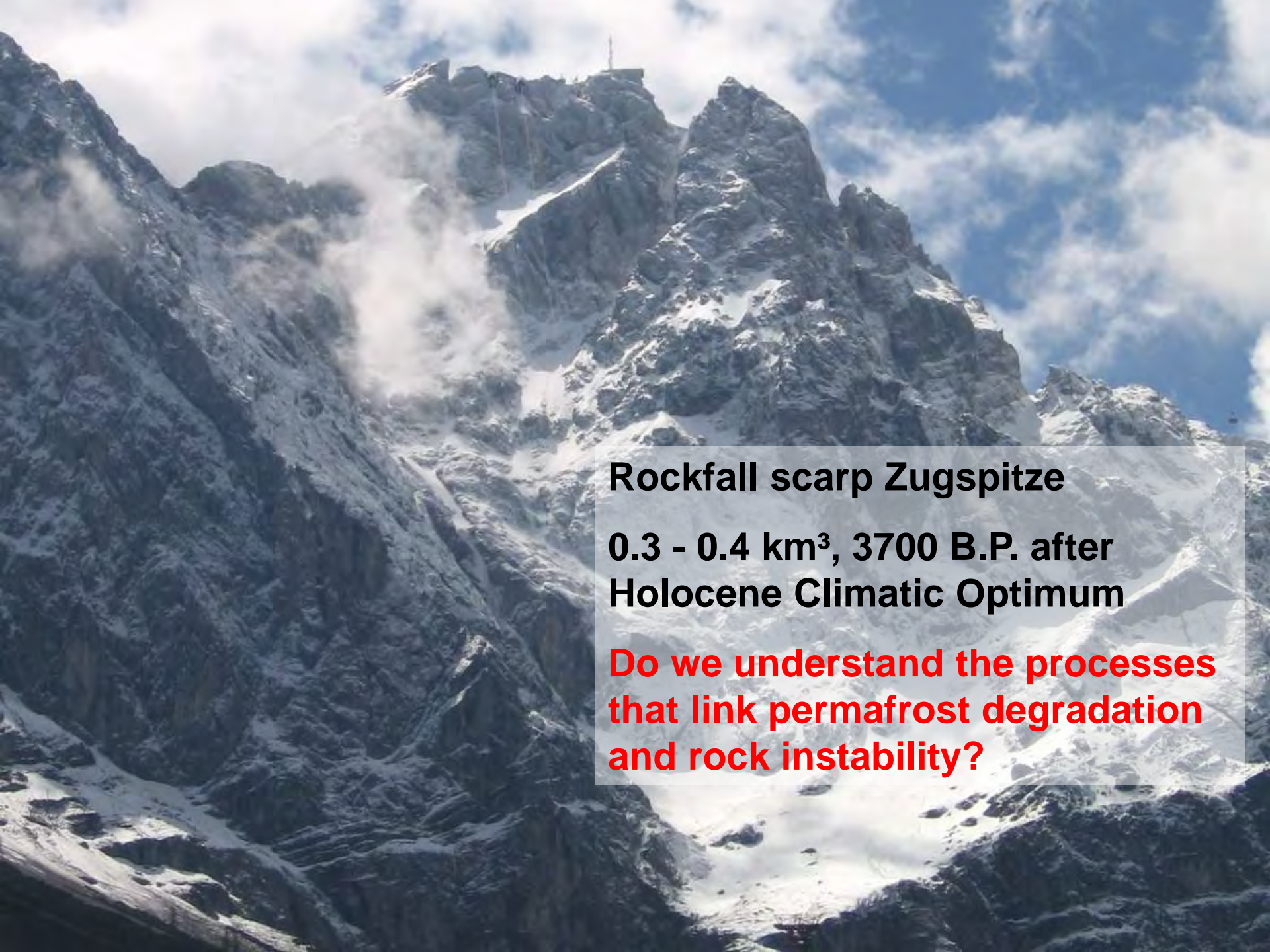
Festsymposium Professor Dr. - Ing. Heinrich Kreuzinger

Michael Krautblatter

**Fachgebiet Hangbewegungen
Ingenieur fakultät Bau Geo Umwelt
Technische Universität München**

Abschätzung zukünftiger Naturgefahren:

1. Degradierung Permafrost
2. Murgangaktivität
3. Steinschlagaktivität

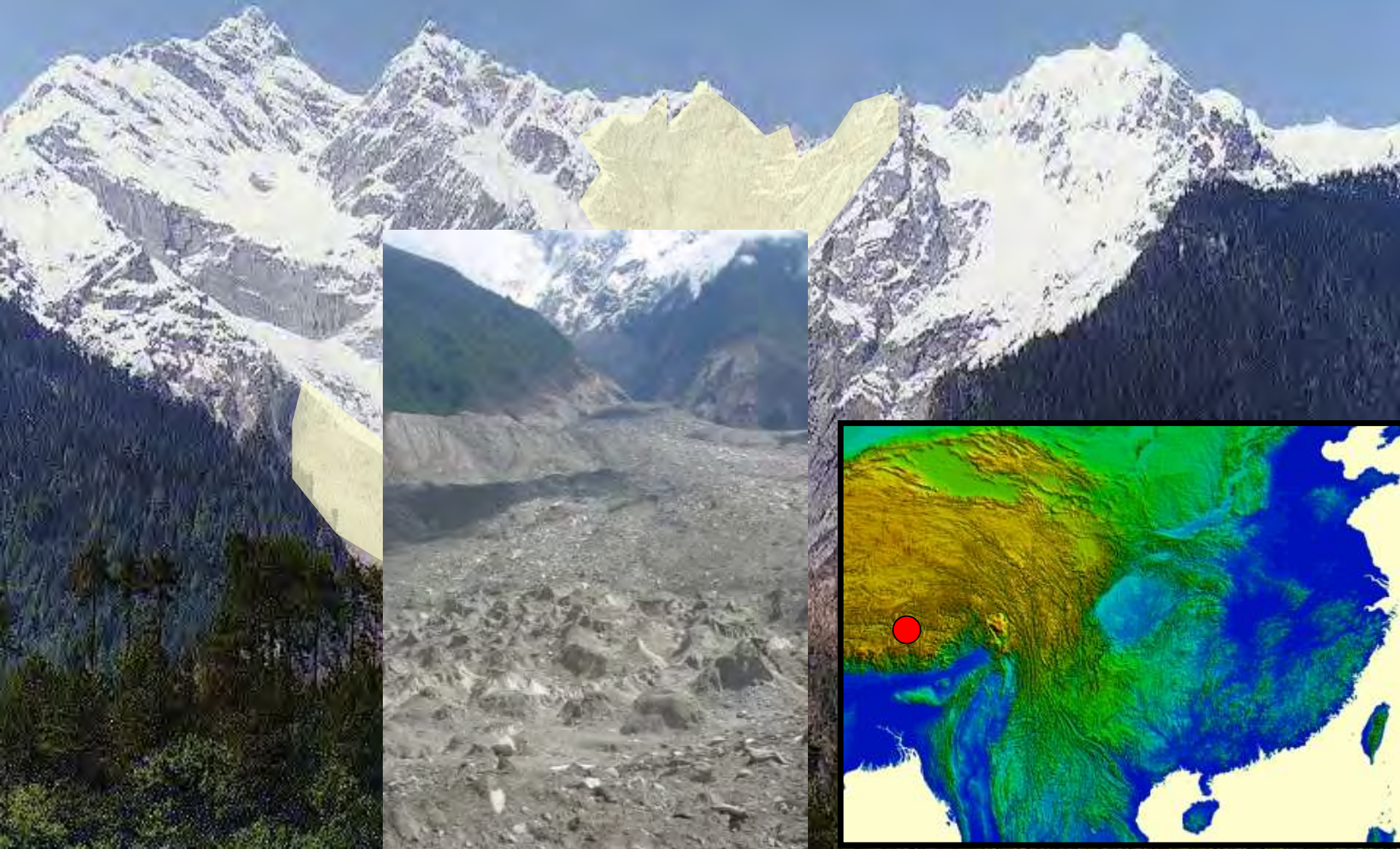


Rockfall scarp Zugspitze

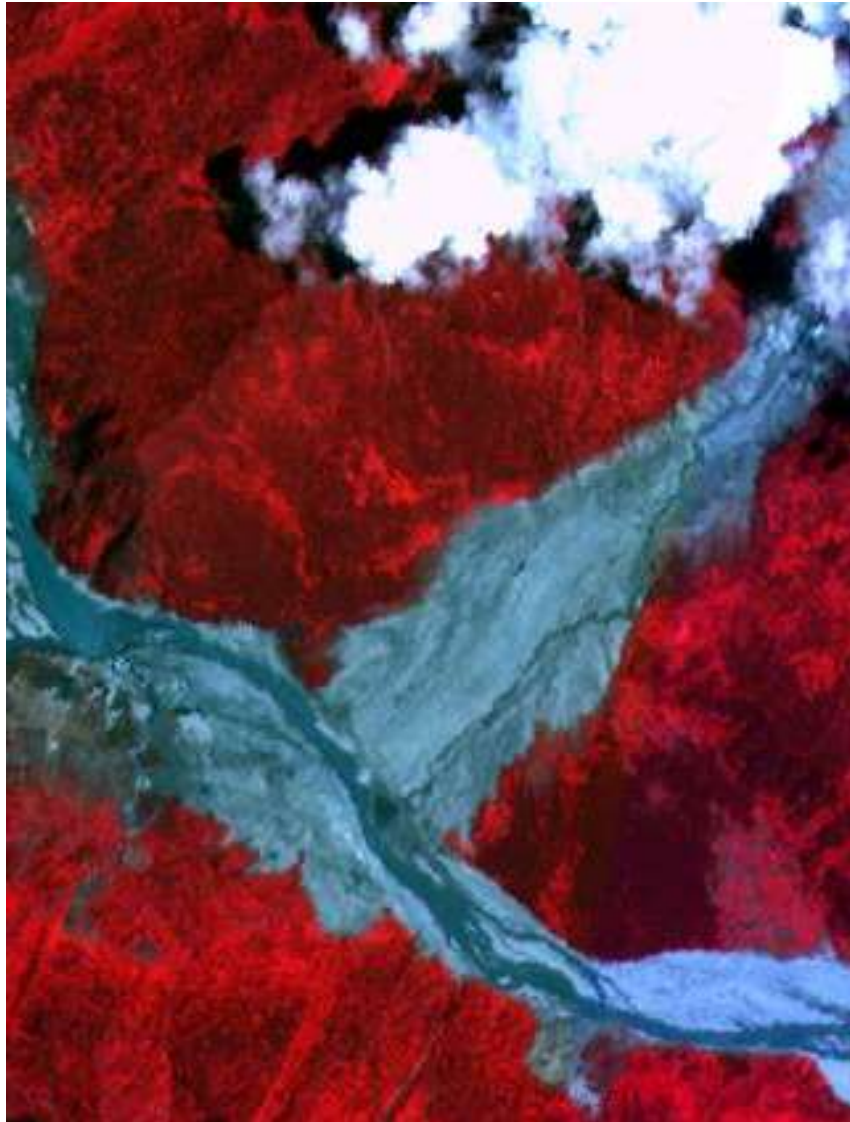
**0.3 - 0.4 km³, 3700 B.P. after
Holocene Climatic Optimum**

**Do we understand the processes
that link permafrost degradation
and rock instability?**

Yigong Rock Avalanche April 2000 (Foto by Runqiu Huang)



Hazard due to the 2000 Yigong (Bomi, Tibet, China) rock avalanche



Rock slope failure: April 9, volume 0.28 km³

Landslide dam: 60-100 m high

Blocking of Yigong Zangbo River

Upstream flooding: affected 4000 people, several schools/villages & Yigong tea garden

Channel construction May 3-June 3: 1000 m long, 150 m wide top, 24 m deep, 1.4 mio m³

Catastrophic breach starting June 10

Max. discharge June 11: discharge 120,000 m³/s at Tongmai bridge 17 km downstream, water level 34 m above bridge deck

Flood distance: 216 km China, 284 km India, flash flood 450 km downstream 5 m high

Effects (India): >20 bridges destroyed (including steel suspension bridges), > 50000 people rendered homeless

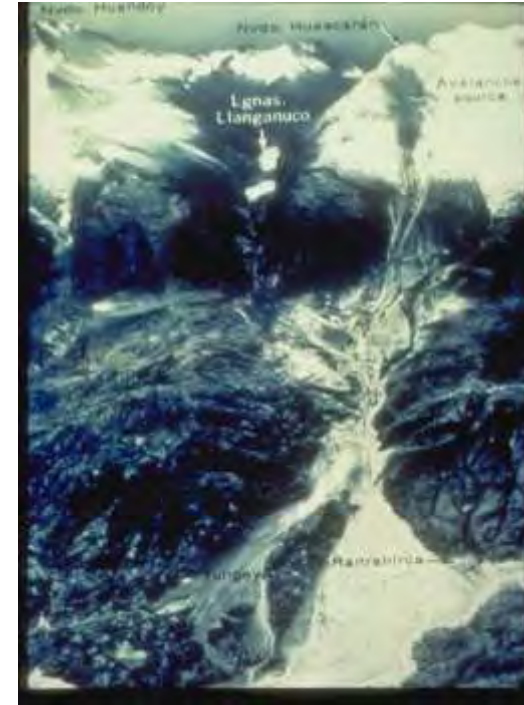
Rock slope failure in permafrost rock walls



*Kolka-Karmadon rock-/ice avalanche
(Russ. Caucasus 2002, 100 mio. m³)*

140 casualties

Huggel et al. 2005



*Huascarán rock-/ice avalanche
(Peru 1970, 50-100 mio m³)*

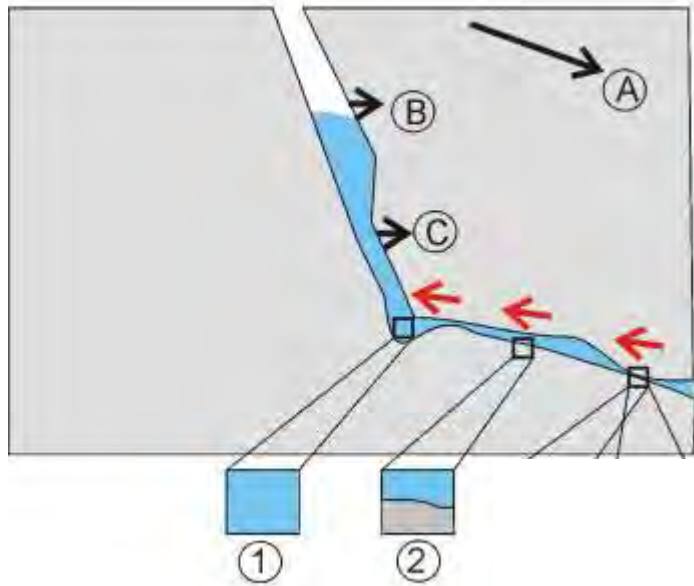
20.000 casualties

Erismann and Abele 2001

Rock creep in permafrost rocks



*Deformation Gipfelseilbahn
(Gemsstock, Andermatt, CH)*



Shear force

- A. gravitational force
- B. hydrostatic pressure
- C. ice segregation

Shear resistance

- force needed for
1. creep and fracture of ice itself
 2. fracture along rock-ice contacts

Davies et al. 2003/Fischer et al. 2006

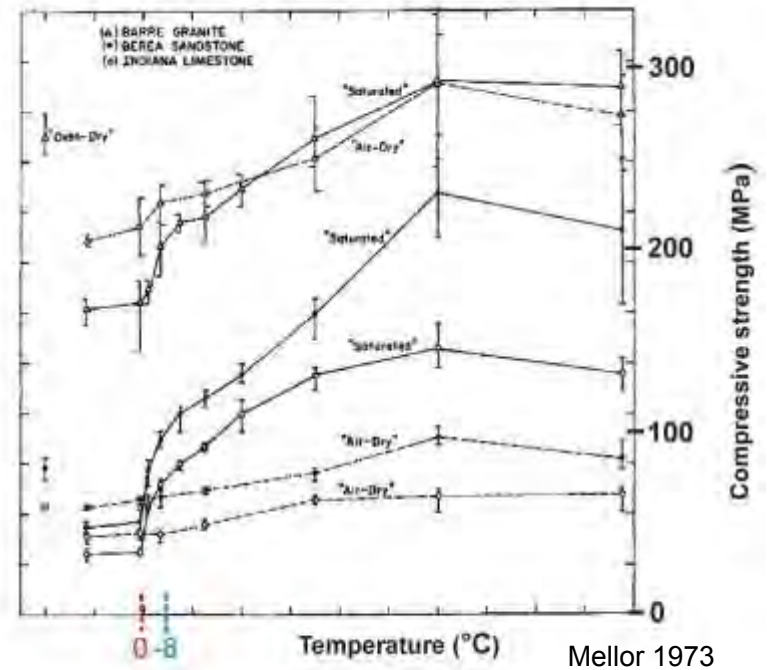
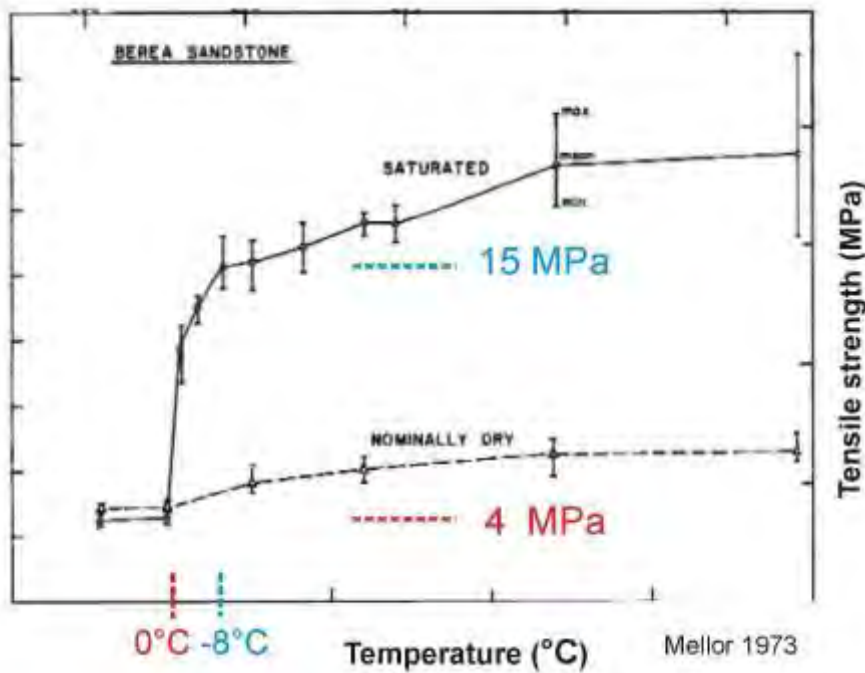
Murton et al. 2006/ Gruber & Haeberli 2007

Davies 2000/Arenson & Springman 2005

Guenzel 2008

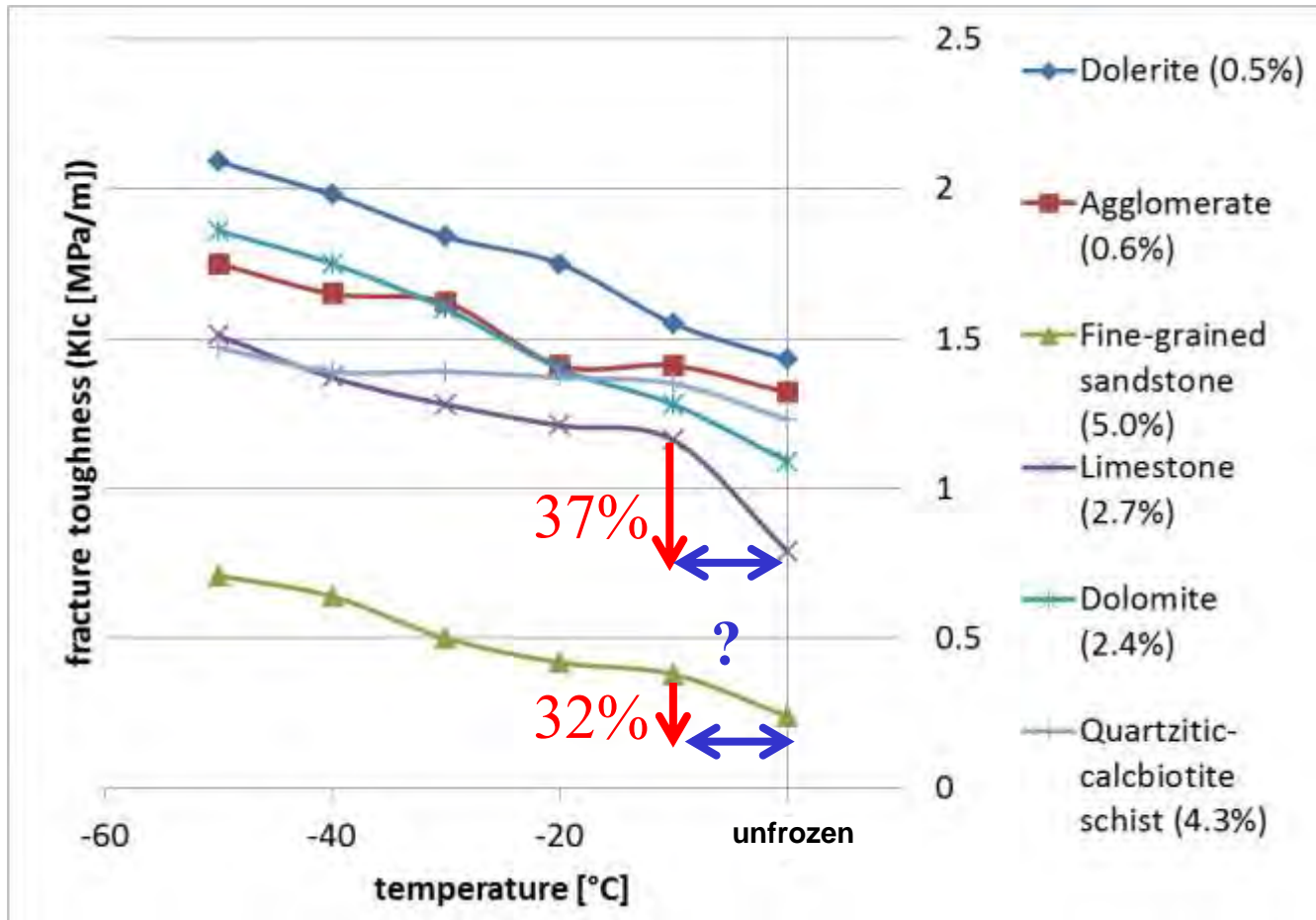
1. Why/How does thawing affect rock-mechanical properties (friction/fracturing)?
2. At what time and spatial scales of destabilisation do rock- or ice-mechanical processes dominate instability behaviour?
3. Empirical evidence for rock mechanical destabilisation when thawing?

Compressive and tensile rock strength during thaw



- Compressive and tensile strength of saturated intact rock decrease by 25-75% when thawing (Mellor 1973).

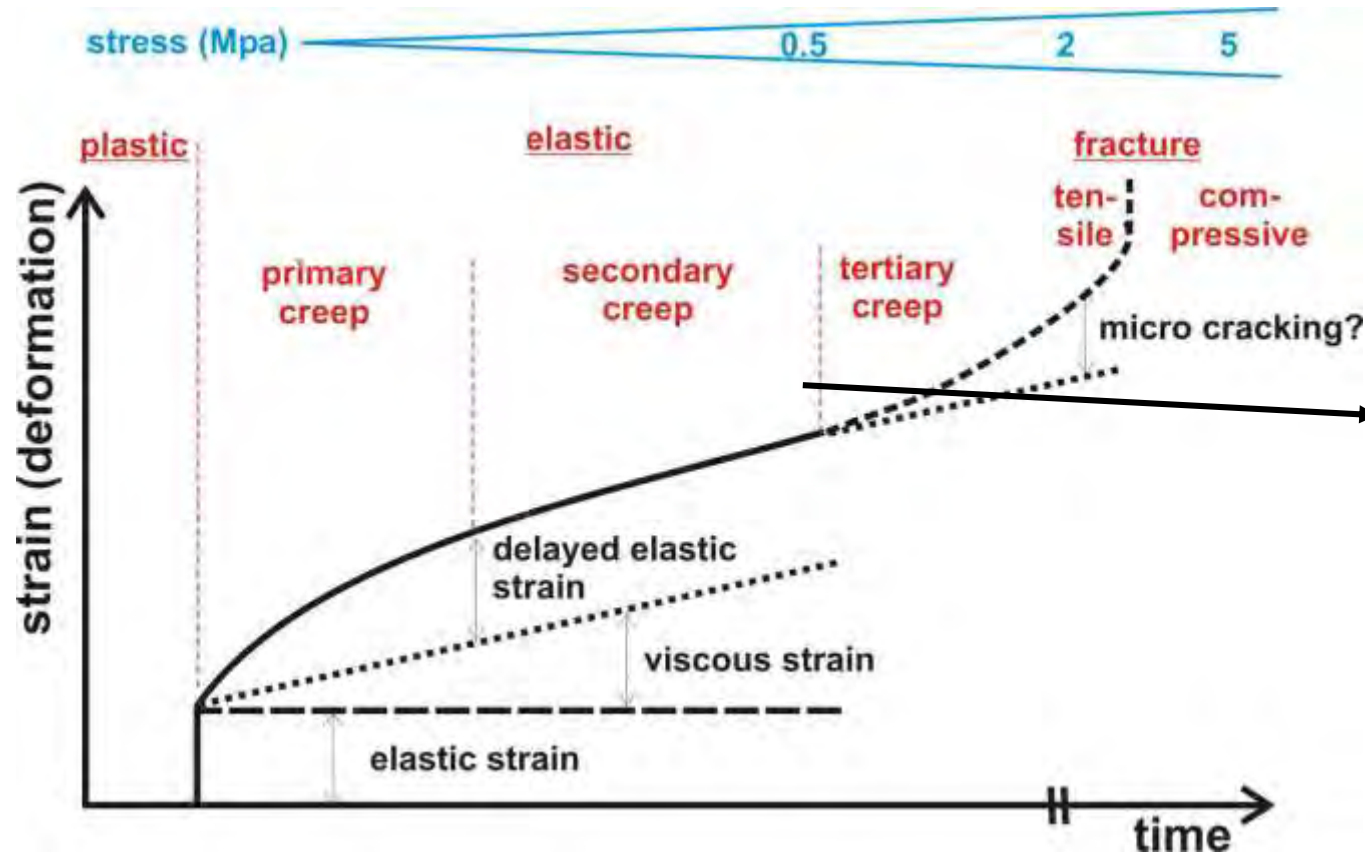
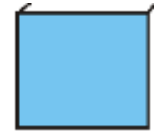
Fracture toughness during thaw



Dwivedi et al. 2000

- Fracture toughness in water-saturated rocks decreases by up to 40% when thawing (Dwivedi et al. 2000)
- This effect is more pronounced for repeated freezing (Inada&Yokota 1984)

Shear resistance of ice itself



$$\tau_{xy}^n = \dot{\epsilon}_{xy} / A$$

$\dot{\epsilon}_{xy}$ strain rate

τ_{xy} shear stress

- At very low velocity (i.e. strain rate), at which e.g. subcritical cracking of rock bridges occurs, the shear resistance of ice due to creep is negligible.
- Fracturing only occurs at higher velocities (strain rate $>10^{-3} \text{ s}^{-1}$; Sanderson, 1988).

A preliminary rock-ice mechanical model

$$|\tau| = \frac{K_c \sqrt{\pi a}}{2w}$$

fracture of rock bridges

$$+ \sigma' \tan(\varphi + JRC * \log_{10}(\frac{\sigma_c}{\sigma'}))$$

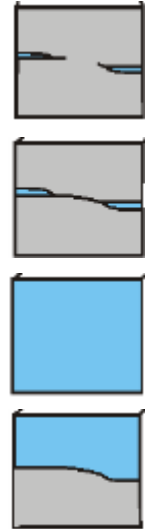
total friction due to fracture roughness

$$+ \frac{\varepsilon_w}{A_v \exp(-\frac{16700}{T})}$$

reduction of effective shear stress due to secondary/tertiary creep of ice

$$+ (-145 * T_c + 0.47 * \sigma' - 3.5)$$

failure criterion of ice in rock clefts



Dynamic components (yellow):

$|\tau|$ shear stress at failure, K_c critical fracture toughness, σ_c compressive strength and temperature T_c [°C] und T [K]

Processes act individually, in succession or in combination

Destabilisation in time

$$|\tau| = \frac{K_c \sqrt{\pi a}}{2w}$$

fracture of rock bridges

$$+ \sigma' \tan(\varphi + JRC * \log_{10}(\frac{\sigma_i}{\sigma'}))$$

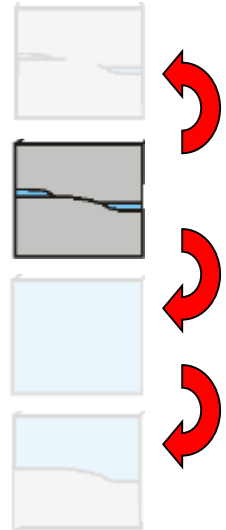
total friction due to fracture roughness

$$+ \frac{\varepsilon_w}{A_0 \exp(-\frac{16700}{T})}$$

reduction of effective shear stress due to secondary/tertiary creep of ice

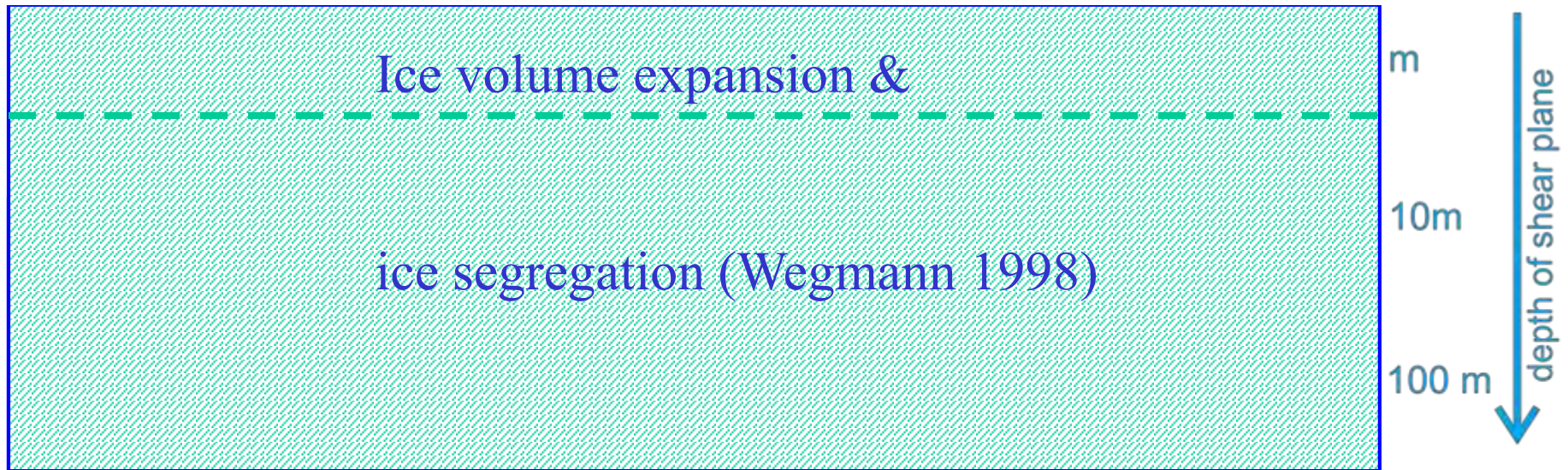
$$+ (-145 * T_c + 0.47 * \sigma' - 3.5)$$

failure criterion of ice in rock clefts



- At very **low velocities** (strain rates) **rock-mechanical** processes dominate initial destabilisation.
- Only at **higher velocities** **ice-mechanical** outbalance the importance of rock-mechanical processes.

Destabilisation in space

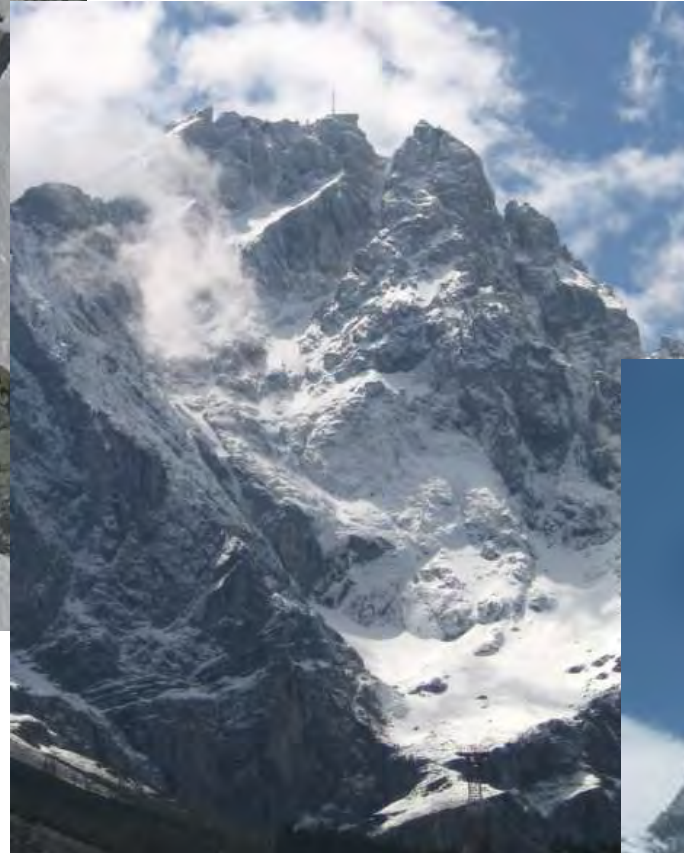


Restriction:

Sample sites



Steintälli, Mattertal, CH



Zugspitze, D/A



Kitzsteinhorn , A

Non-destructive and destructive testing techniques



Non-destructive:

- P- wave velocity
- S-wave velocity
- >Elastic moduli



Destructive:

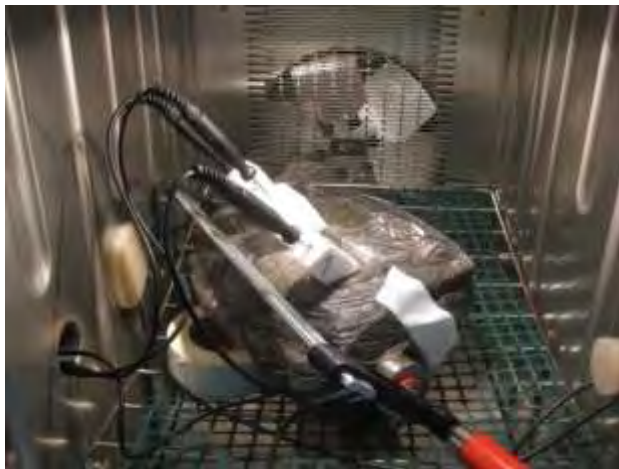
- Compressive strength (Uniaxial)
- Tensile strength (Brazilian)

Inhomogeneity, scale and anisotropy



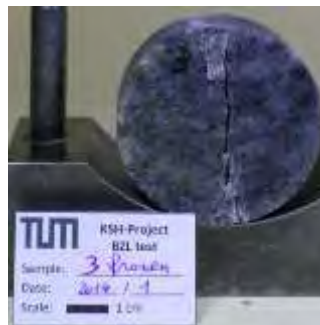
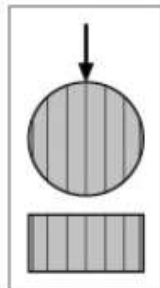
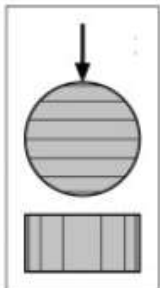
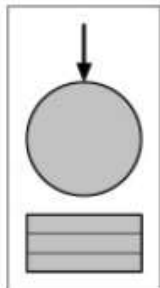
Inhomogeneity

Statistic amounts of samples



Scale:

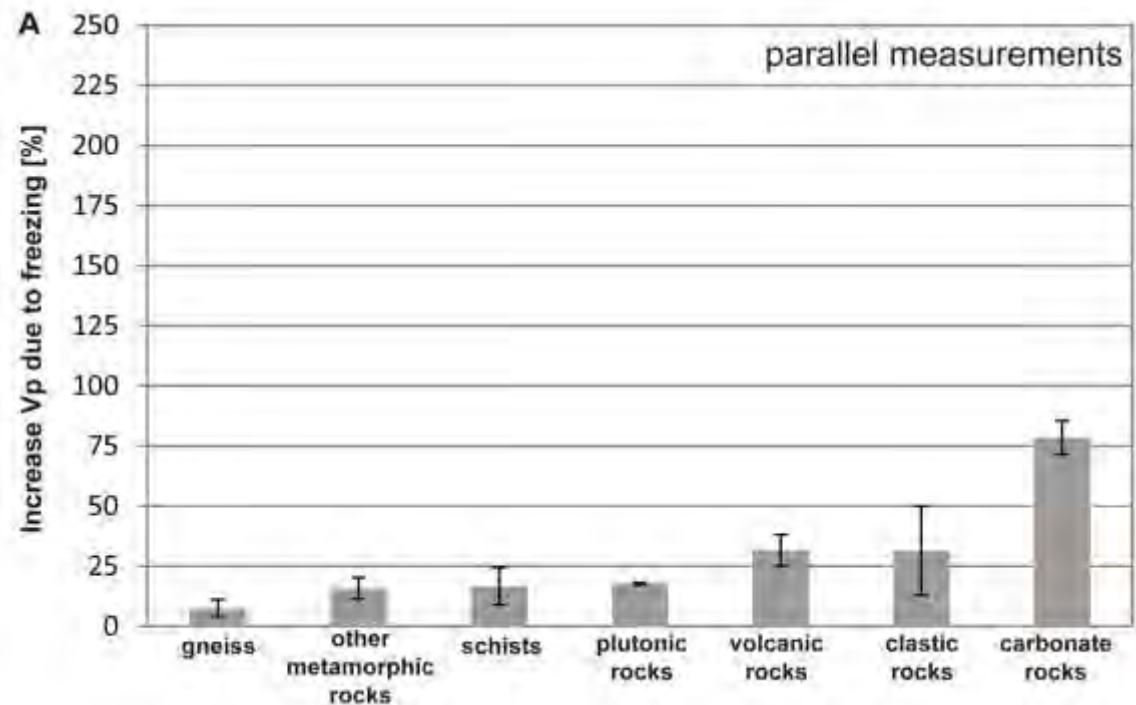
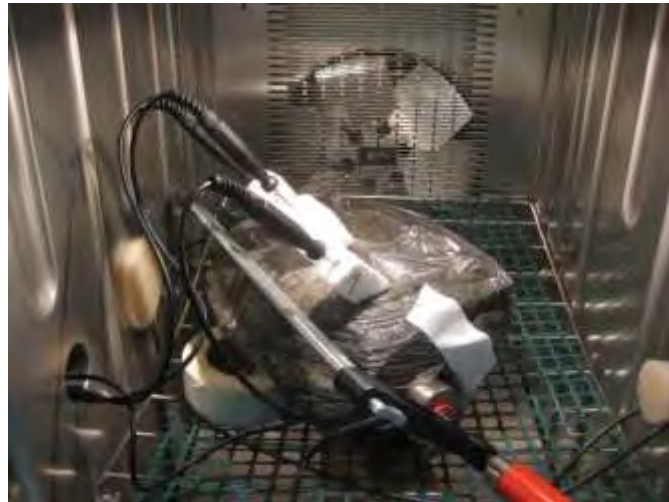
Differing testing scales with respect to fracture patterns or surface roughness



Anisotropy:

Differing testing directions with respect to fracture/schistosity orientation

Increase in fracture toughness: P-Wave velocity as a proxy



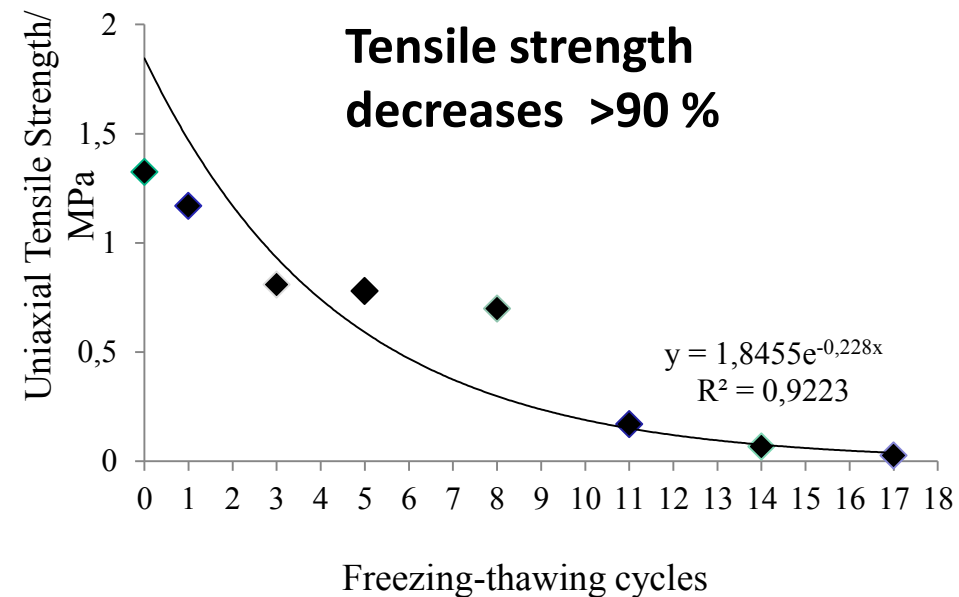
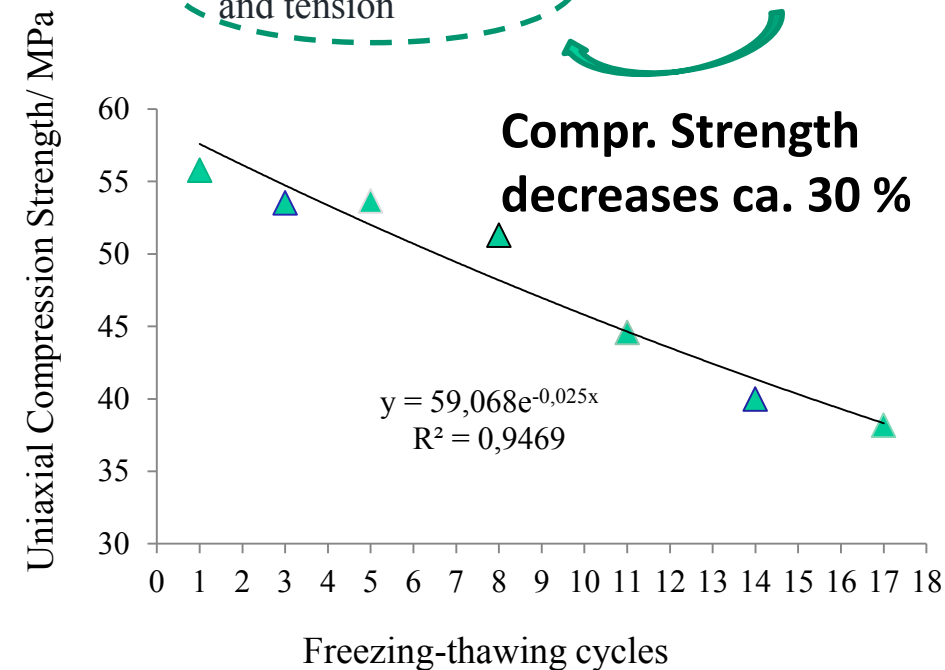
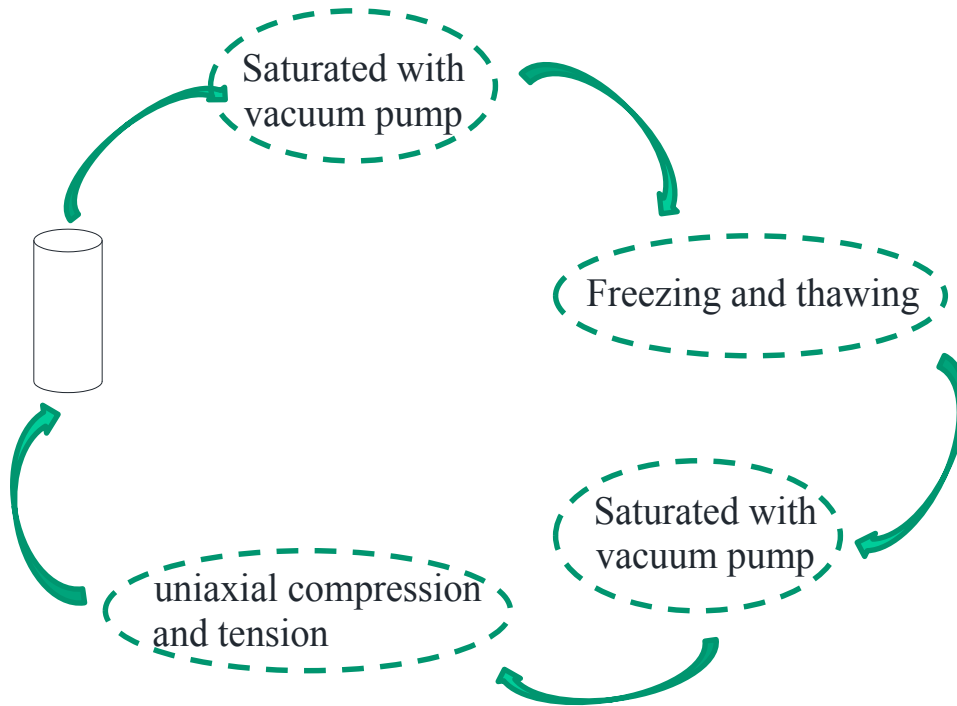
P-wave velocity is the best correlated factor with K_{Ic} fracture toughness (Chang et al. 2002, $R^2=0.8$).

P-wave velocity can be measured non-destructively and in different directions.

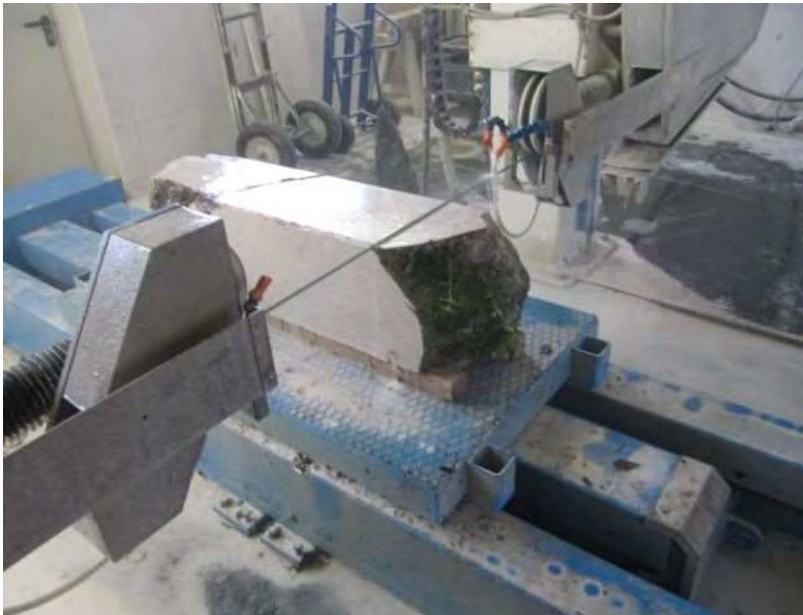
High-resolution (0.2°C increments) changes in P-wave velocity were measured in 22 alpine and arctic rock samples (Dräbing & Krautblatter, 2012, *The Cryosphere*)

3D - Field application (Krautblatter&Draebing, 2014)

Fatigue: Reducing mechanical strength upon repeated freezing



Field-lab analogue testing



Experimental setup: 4 soft chalk blocks, 2 Wetterstein limestone blocks



Instrumentation on each block



Instrumentation:

- 32 galvanic electrodes for ERT
- 32 copper plates for capacitive EIT
- 8 TDR sensors (rock moisture)
- 8 platinum temperature sensors
- 1 heave sensor (0.01 mm)
- 1 geophone (1000 Hz, cont. recording)

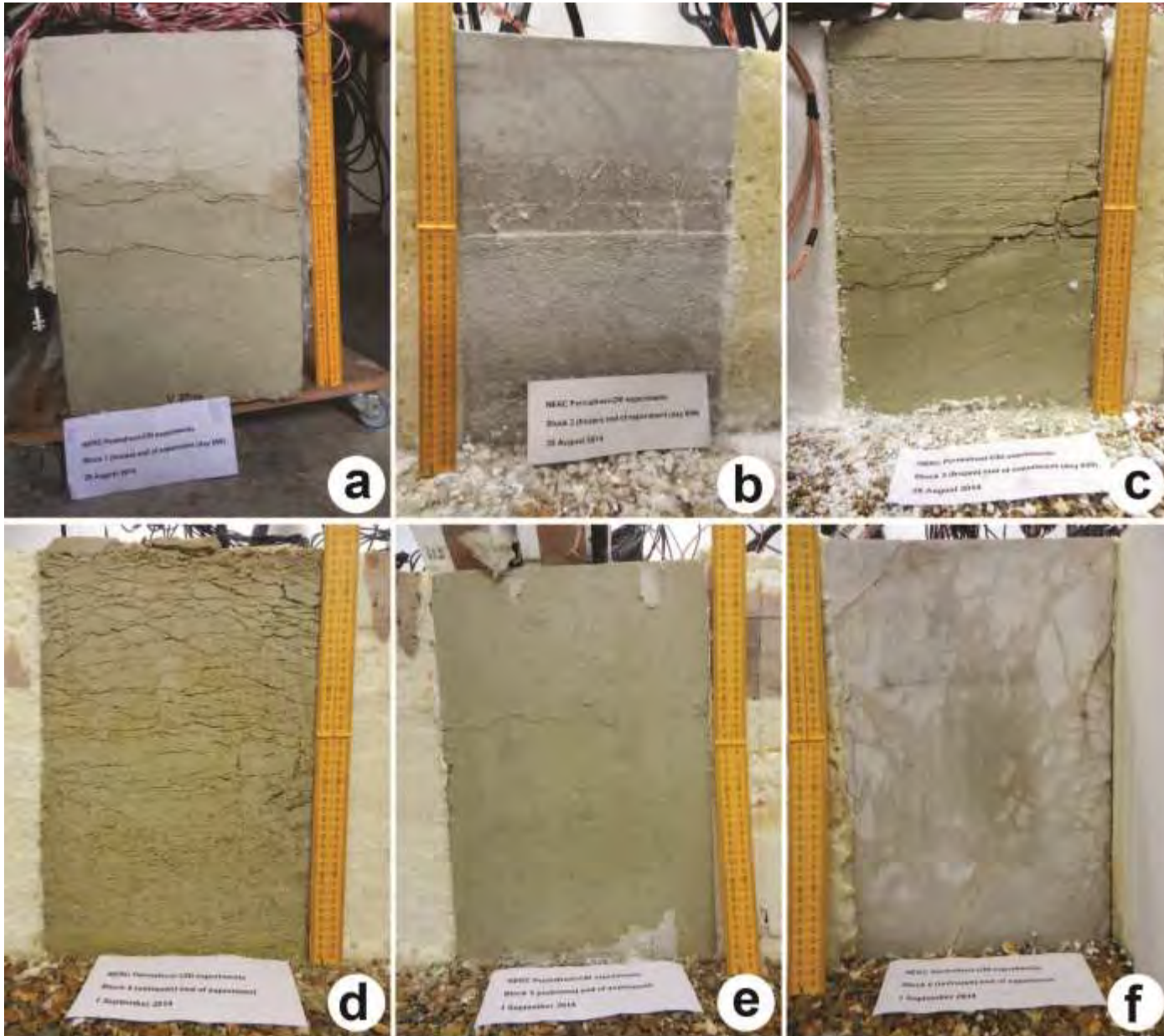
Schedule:

- Installation: April 2011 – April 2012
- Start of test: April 25, 2012
- Duration: 900 days - 2015

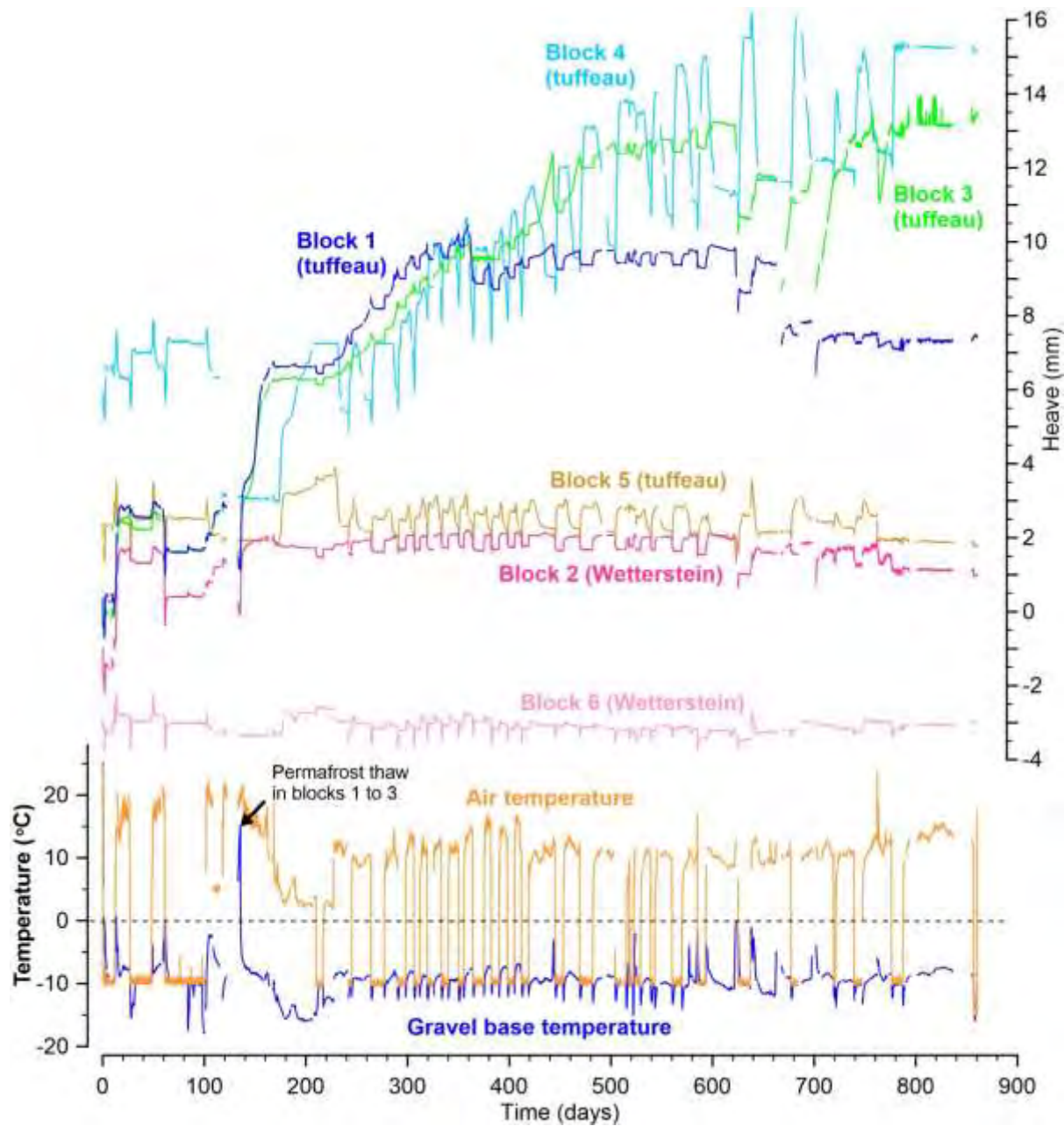
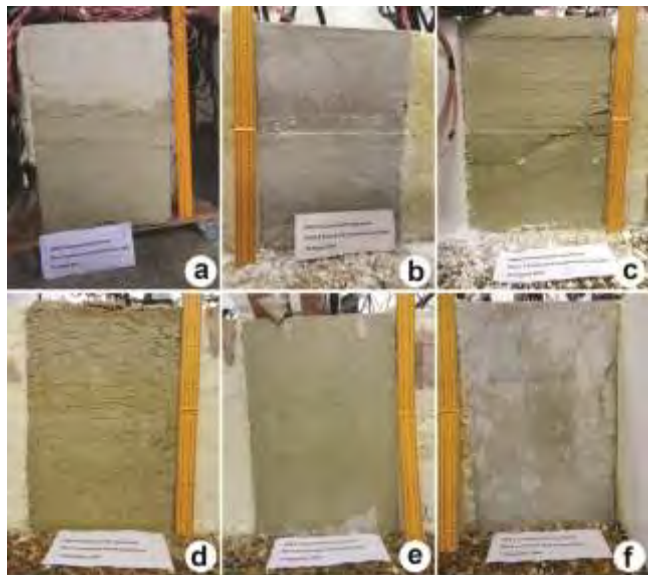
Project: CRI-Permafrost, NERC:

Prof. J. Murton, U. of Sussex,
Dr. O. Kuras, Brit. Geol. Survey
Dr. M. Krautblatter, TUM

900 days, > 20 freezing cycles and resultant shattering



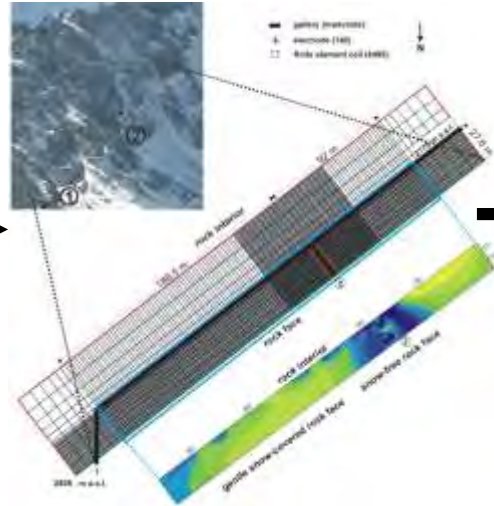
Heave signal



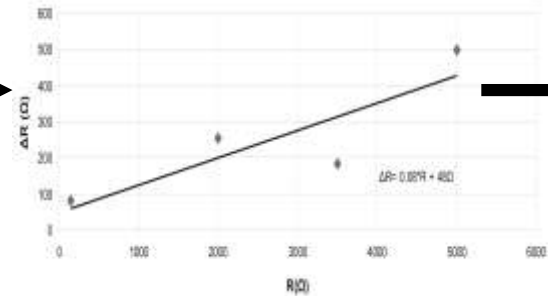
Quantitative ERT (Zugspitze, 2800 m a.s.l.)



High-res. resistivity measurement (3000 datums)



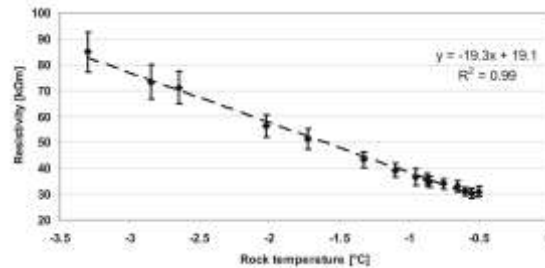
Finite element grid



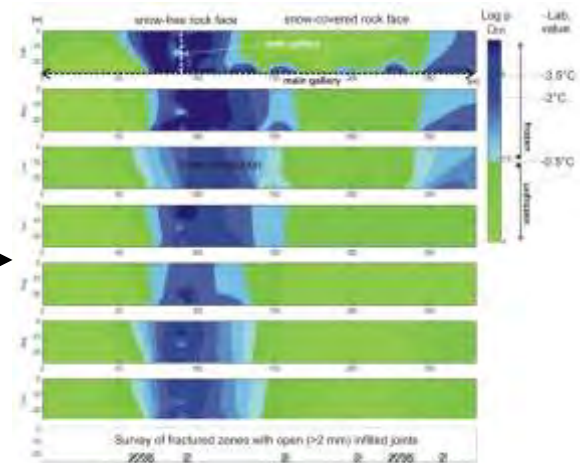
Empirical error model



Laboratory calibration

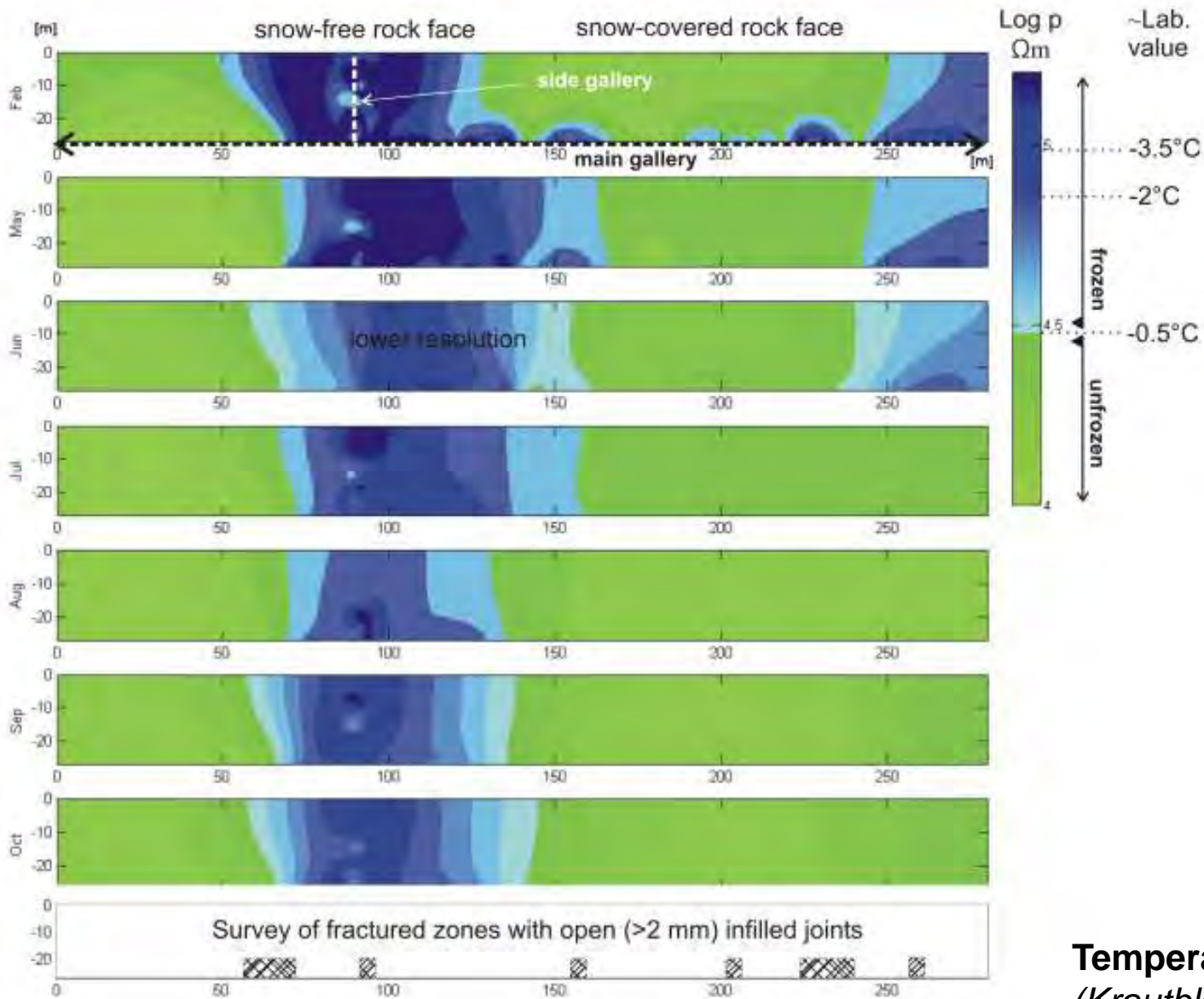


Temperature-resistivity function



Temperature-calibrated ERT (Krautblatter et al. 2010 JGR)

Quantitative ERT (Zugspitze, 2800 m a.s.l.)



Temperature-calibrated ERT
(Krautblatter et al. 2010 JGR)



Field work



Transects Aguille du Midi (3842 m a.s.l.)

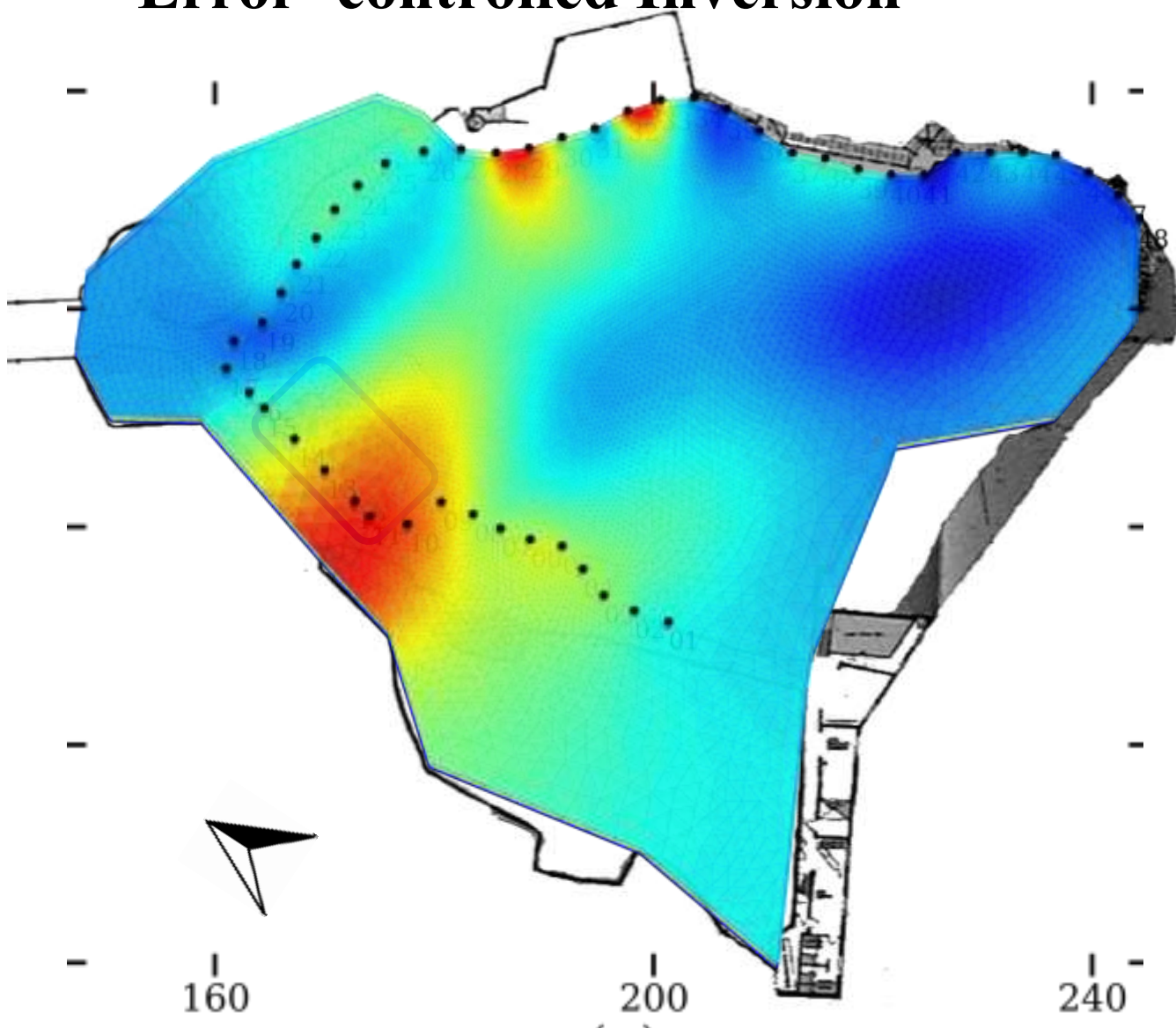
Measurements

- Dec 2008
- Jun 2009
- Oct 2009
- Oct 2010

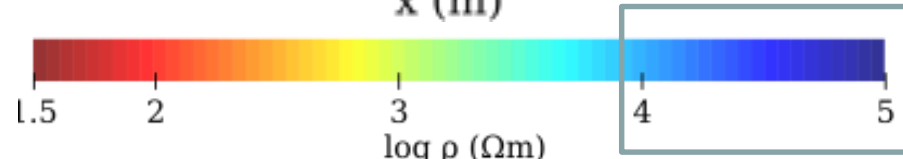


Error- controlled Inversion

Piton Central
Oct 2010

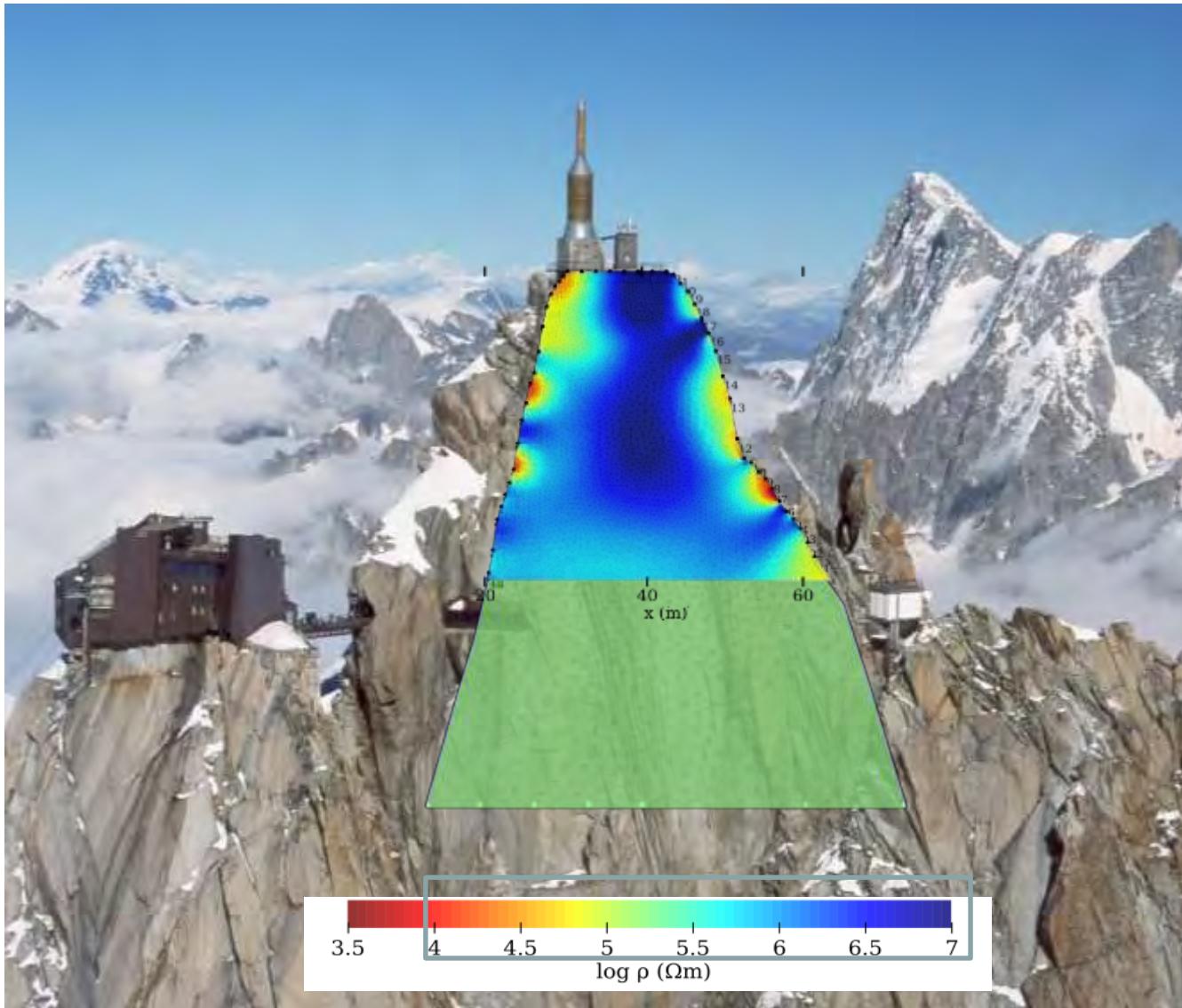


- Skip 3
- Robust inversion
- Rel. error: 26,97 %
- Abs. error: 0,12 Ω
- Background resistivity: 10.000 Ωm
- Electrode gap 12-15 (storage room)
- 318 datum points



Piton Central

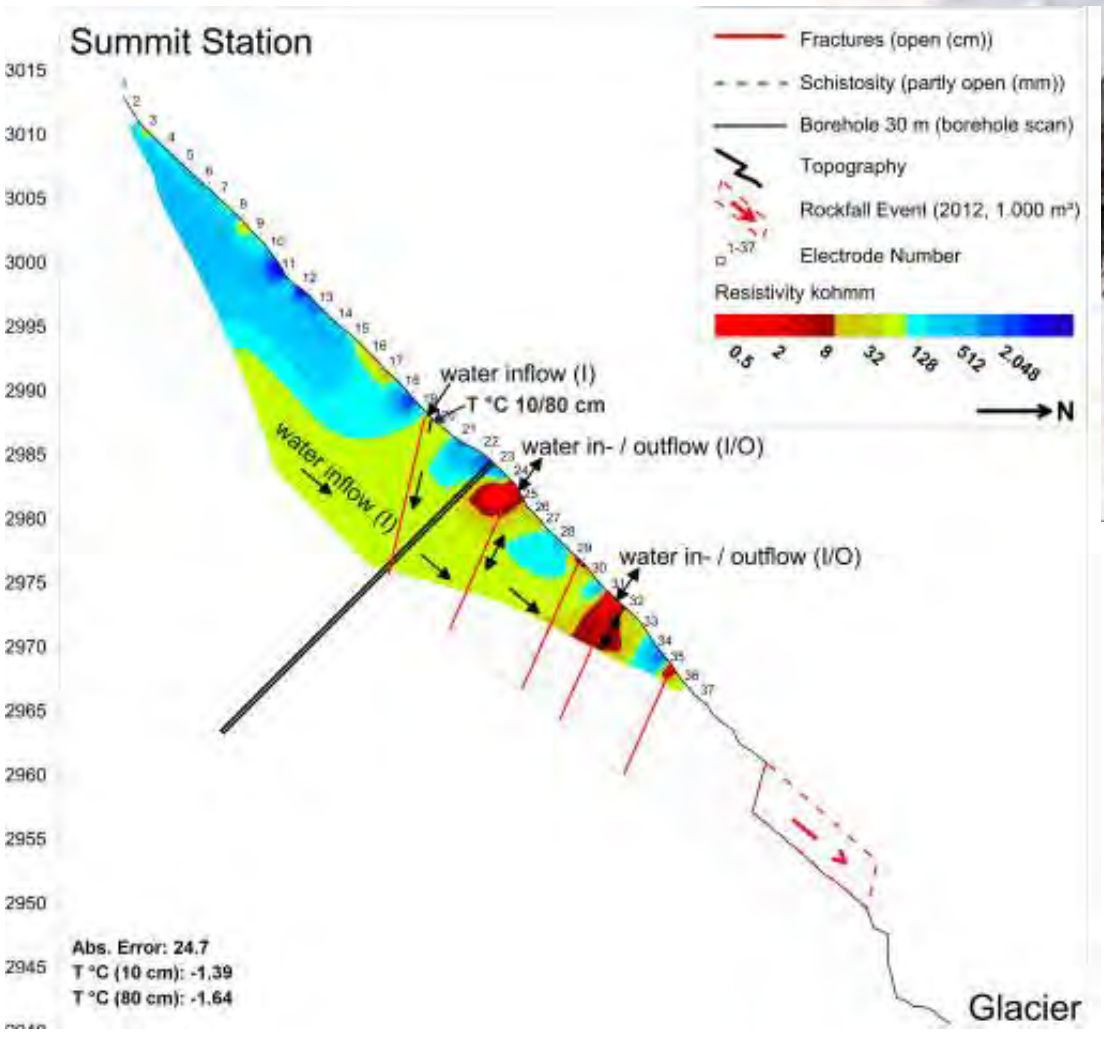
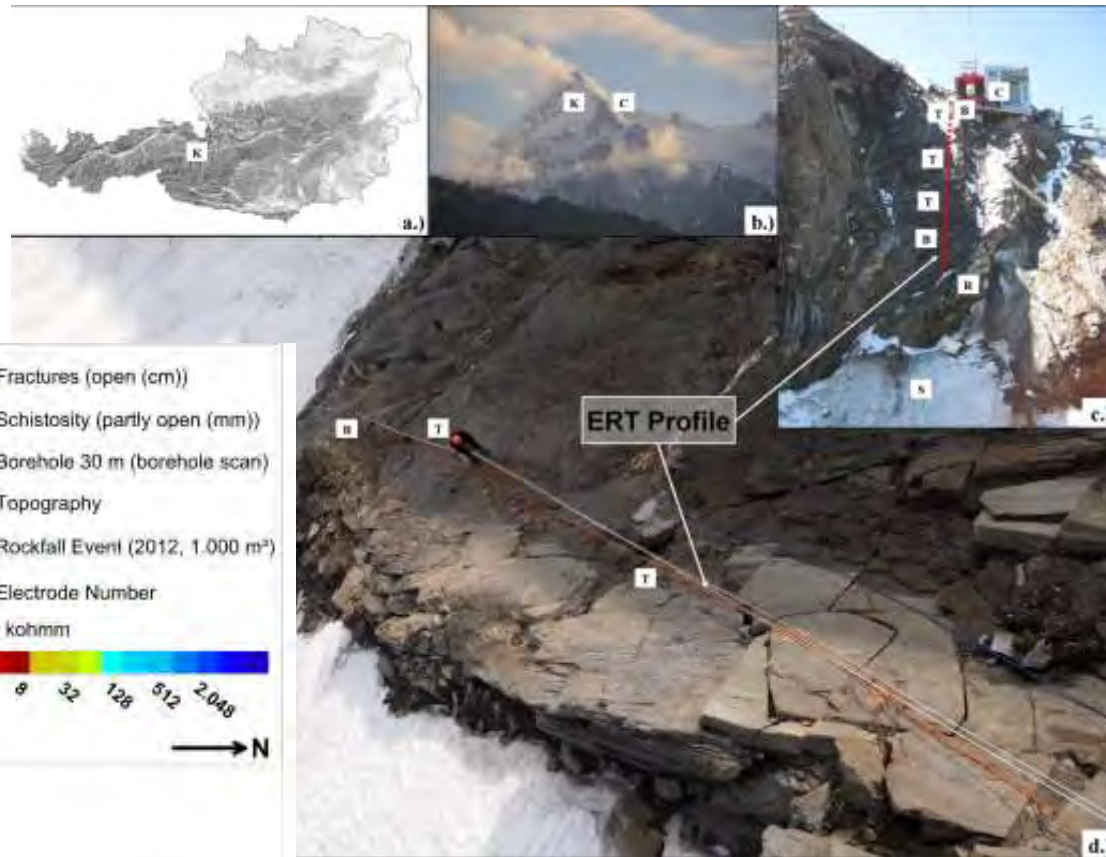
Oct 2010



Altered Colour Scale!

- Skip 3
- Robust inversion
- Rel. error: 36,19 %
- Abs. error: 23,07 Ω
- Background resistivity: 10.000 Ωm
- 156 datum points

Continuous ERT monitoring for cable car infrastructure



**Keuschnig,
Krautblatter et al. (in
review), PPP**

Deriving a model of permafrost-related rock slope failure

Mechanical failure model



Fig. 4: Study site with profile used for modelling.

- first modelling results: higher xy-displacements and lower factor of safety for „unfrozen condition“ (fig. 5)
- next step 1: assign „frozen material parameter“ to frozen zones identified by i) geophysics (ERT, SRT) and ii) direct rock temperature monitoring (fig. 6, right)
- next step 2: calculate with complex topography and joint set configuration

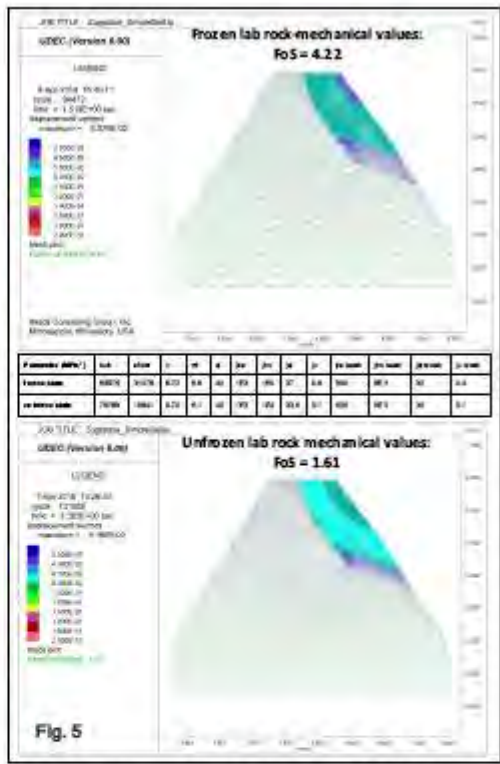
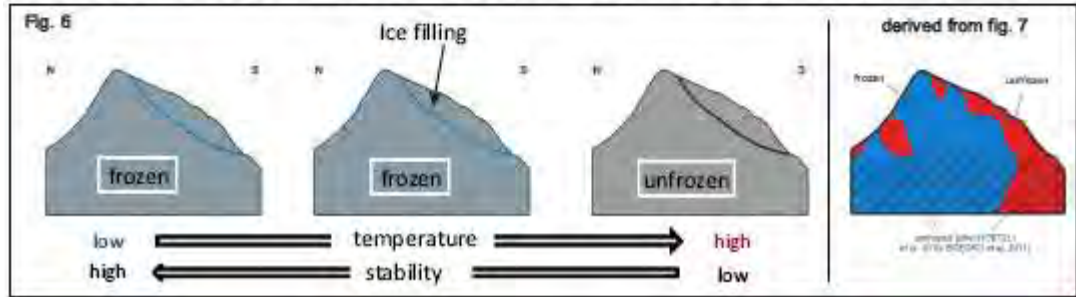


Fig. 5: Two UDEC models with simple geometry of the Zugspitze crest, displacement vectors (in meters) and calculated factors of safety for frozen (above) and unfrozen conditions (below).

Fig. 6: Sketch of the same rock slope as in fig. 5 with various temperature - stability states corresponding to modelling results in fig. 5.



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